Transport and Fate III

Model Simulation of the Long-term Environmental Fate and Profile Transformation of Polychlorinated Dibenzo-p-Dioxins and Polychlorinated Dibenzofurans by the Dynamic Multimedia Environmental Fate Model

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Introduction

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The environmental fate of polychlorinated dibenzo-*p*-dioxins and polychlorinated dibenzofurans are not still clear, because many processes could have complex contribution in the environment. Homologue profiles and/or congener patterns are utilized for the study on the fate of the compounds, together with the simple mass-balance approach. However, a modeling approach, which could combine the possible environmental processes into a system, could be a useful complement for the analytical study on the fate of the compounds¹.

In this study, a dynamic multimedia environmental fate model of PCDD/PCDF was developed for the Japanese environmental condition. Dynamic modeling was necessary to include temporal emission from impurities in pentachlorophenol (PCP) and chlornitrofen (CNP), and to simulate the long-term change of environmental levels and transformations as the result of the emission control of municipal solid waste incinerator (MSWI) and others. A monte-carlo simulation was also performed to examine the sensitivity of the model to the parameter fluctuation.

Methods

Model formulation

Dynamic multimedia environmental fate model was developed based on the fugacity level IV model², which was the extension of the steady-state level III model³. Ten unit models, each corresponding to one of ten 4 to 8 chlorine substituted PCDD/PCDF homologues, were prepared as previously reported⁴. The formulation was as follows:

$$V_{1}Z_{B1}(df_{1}^{j}/dt) = E_{1}^{j} - f_{1}^{j}D_{T1}^{j} + f_{2}^{j}D_{21}^{j} + f_{3}^{j}D_{31}^{j} + f_{1}^{j+1}D_{R1}^{j+1}$$
(Air, *i*=1)

$$V_{2}Z_{B2}(df_{2}^{j}/dt) = E_{2}^{j} + f_{1}^{j}D_{12}^{j} - f_{2}^{j}D_{T2}^{j} + f_{3}^{j}D_{32}^{j} + f_{4}^{j}D_{42}^{j} + f_{2}^{j+1}D_{R2}^{j+1}$$
(Soil, *i*=2)

$$V_{3}Z_{B3}(df_{3}^{j}/dt) = E_{3}^{j} + f_{1}^{j}D_{13}^{j} - f_{3}^{j}D_{T3}^{j} + f_{3}^{j+1}D_{R3}^{j+1}$$
(Water, *i*=3)

$$V_{4}Z_{B4}(df_{4}^{j}/dt) = E_{4}^{j} + f_{2}^{j}D_{24}^{j} - f_{4}^{j}D_{T4}^{j} + f_{4}^{j+1}D_{R4}^{j+1}$$
(Sediment, *i*=4)

where, E_i^j : emission rate of homologue j to the compartment i; f_i^j : fugacity of homologue

ORGANOHALOGEN COMPOUNDS Vol. 36 (1998) *j* in the compartment *i*; $D_{ii'}^j$: transportation parameter; D_{Ri}^j : degradation parameter of homologue *j* in the compartment *i*; *j*: homologue number; Z_{Bi} : bulk phase Z values.

The term $f_i^{j+1}D_{Ri}^{j+1}$ was introduced to express the degradation of the homologue with j+1 chlorine substitution to the homologue with j chlorine substitution. All modeling effort was performed on the homologue total amount basis.

Physical/chemical and environmental data

Most of the parameters were estimated by the previous method⁴ from literature data^{5,6}. Emissions from impurities in PCP and CNP were estimated by literature data. Emission rates from MSWI were assumed to decrease after 1995 by regulation or controlling measures. Figure 1 shows the assumed emission rates of total PCDD/PCDF from the three sources.

Flux of soil particles into air due to wind erosion

Flux of soil particles into air by wind erosion was formulated as follows:

$$N = U_E \rho_S C_S$$

where, N : flux of dioxins due to soil particles into the air by wind erosion $(mg/m^2 \cdot h)$; U_E : wind erosion velocity (m/h); ρ_S : Density of soil particles (kg/m^3) ; C_S : dioxin concentration in soil particles (mg/kg).

The flux N was then incorporated into D values of the formulation. Parameter U_E was determined to obtain the fixed mixing ratio of soil particles in the total air particles (x). Central estimate of x was set to 0.3 based on the result of the receptor modeling⁷.

Sensitivity analysis

Target parameters of monte-carlo analysis were assumed to follow log-normal distribution with standard deviation corresponding to 2-fold variance from central estimates, with some exceptions according to the nature of parameters. Standard deviations of fugacities were calculated from 1000 times trials for each parameter. The results were expressed as the ratio of input standard deviation to the output standard deviation, σ_{aw}/σ_{in} .

Results and Discussions

Simulated environmental levels and model validation

Table 1 shows the description of cases 1 to 5, which examine the effect of some model processes on the simulation results. Table 2 summarizes the simulated concentration.

Estimated concentration from basic case 1 suggests that the concentration of soil and depositions seem to become closer to the measured environmental concentration and depositions^{8,9,10,11} than the result of the previous report⁴. However, the concentration in air still seems lower, and that in sediment seems higher than the real environmental level^{8,12}.

Figures 2 to 4 show the time trend of fugacities in case 1 for TCDD, OCDD and TCDF, respectively. Figures 2 to 4 suggest that non-steady state environmental condition lasts for

Case 1	Base simulation (Sources=MSWI+CNP+PCP) without Degradation-Emission link
Case 2	Case 1+Degradation-Emission link ($P_nCDD/F \rightarrow P_{n-1}CDD/F$)
Case 3	Omit soil mixing ratio in air from Case 1
Case 4	Steady state simulation (Level III) with Case 1 parameters (Source=MSWI only)
Case 5	Non-steady state simulation with Case 4 parameters (Source=MSWI only)

Table 1 Description of Cases

		Conce	Deposition				
	Air	Water Soil		Sediment	Dry	Wet	
	$\left(pg/m^{3}\right)$	(pg/l)	(pg/g)	(pg/g)	$\left(ng/m^2 \cdot y\right)$	$\left(ng/m^2 \cdot y\right)$	
Case 1	1.8	303	2340	51300	63	113	
Case 2	1.8	339	2630	57600	64	113	
Case 3	1.8	303	2340	51300	63	112	
Case 4	1.6	11	57.4	1999	59	104	
Case 5	1.6	4	20.5	657	59	104	

Table 2 Simulated concentrations and depositions (Total PCDD/Fs) in 1995

several decades, especially for OCDD, which is assumed to have the longest degradation half-lives. Comparison of Figures 2 to 4 to Figure 1 shows that the response of fugacities in sediment is simulated to be delayed maybe for decades from emission input. Fugacities in air, water and soil are simulated to follow more immediately to the emission change. The results suggest the possible long response time to reach steady-state condition, although the assumed degradation half-lives and other parameters could significantly affect this implication.

Effect of process assumptions to the simulation

Comparison of cases 1 and 2, reveals that the degradation-emission formulation has relatively minor importance on the estimated total concentrations in the dynamic simulation. Comparison of cases 1 and 3, and the result of sensitivity analysis for parameter x, suggest that relatively small contribution of soil wind erosion for the air concentration. However, when soil concentration is very high, probably the soil wind erosion could have a significant contribution in the air concentration. Comparison of cases 4 and 5 suggests that the steady-state model give smaller concentration than the dynamic model with similar parameter set.

Sensitivity analysis

Table 3 shows the examples of σ_{out}/σ_{in} values for parameters with significant sensitivity.

Degradation half-lives in soil may have most significant sensitivity for all homologues, which is suggested by the large σ_{out}/σ_{in} values in Table 3. Scavenging ratio, Q, may be another uniquely sensitive parameter, which give fluctuations in relatively wide range of media and homologues. In other parameters, geographical assumption like the height of air compartment, and some parameters controlling the partition in the media like organic carbonwater partition coefficient, give relatively large σ_{out}/σ_{in} values mainly for the concentration in the corresponding media.

Long term trend in environmental homologue profiles Figures 5 to 7 show the simulated homologue profiles in air for case 1. Long-term change of

Parameter	Media	Year	TCDD	PeCDD	HxCDD	OCDD	TCDF	PeCDF	HxCDF	OCDF	
Half Life	Soil	1975	0.27	0.41	0.35	0.11	0.63	0.52	0.46	0.22	
in Soil		1995	1.71	0.52	0.44	0.33	0.78	0.68	0.61	0.64	
	Ì	2015	3.45	1.32	1.17	0.55	1.96	1.92	1.73	1.07	
Scaveng-	Soil	1975	0.00	0.19	0.17	0.00	0.38	0.26	0.23	0.00	
ing		1995	0.00	0.25	0.25	0.00	0.40	0.28	0.26	0.00	
Ratio		2015	0.00	0.26	0.25	0.00	0.40	0.28	0.26	0.00	

Table 3 Examples of σ_{out}/σ_{in} value from Monte-Carlo sensitivity analysis

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profile may occur as a result of emission change and transformation processes. Figure 5 to 7 shows that profiles in air could be affected by the soil TCDD concentration.



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