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Degradation of Organic Compounds on Fly Ash: Investigating the Role of the Support

Marina Lasagni, Elena Collina, Massimo Tettamanti, Lucio Forni, and Demetrio Pitea Dip. Chimica Fisica ed Elettrochimica, via Golgi 19, 20133 Milano - ITALY

1. Introduction

Since the detection of polychlorinated dibenzodioxins, PCDDs, and polychlorinated dibenzofurans, PCDFs, in the emissions of Municipal Solid Waste, MSW, incinerators, the formation and degradation reactions of these compounds have been intensively studied¹).

Aim of our research is the study of the degradation and formation reactions of most organic compound on fly ash. A kinetic study of this type requires a tremendous analytical effort. Such a study, even if feasible, is practically impossible, taking a too long time to be completed. On the other hand, the global study has great importance particularly for its practical implications in the treatment and disposal of fly ash.

The solution we are proposing is to study the behavior of organic compounds on fly ash through a global parameter. Of course, specificity will partly be lost, since the model we obtain does not describe in an exact manner the behavior of every compound taken separately. Nevertheless, it is very useful for practical purposes.

As global parameter we have chosen the Total Organic Carbon²⁾ (TOC) content, used to measure the reagents' concentrations.

Experiments are performed on fly ash from MSW incinerators and, to help in the interpretation of the results, on synthetic mixtures of pure compounds on silica gel, SiO_2 , as a model support.

In a preliminary study³) we reported the results of batch experiments on fly ash from MSW incinerators and synthetic mixtures of dibenzofuran, DF, biphenyl, BPh, and activated carbon. In the runs on model systems any catalyst or chlorine source are added to the support. Data for the runs on synthetic mixtures were fitted with a first-order kinetic equation. For the runs on fly ash a mechanism of two simultaneous independent first-order reactions, R1 and R2, was hypothesized and the data were fitted with an iterative procedure. The results led to the conclusion that processes both on the model support and on fly ash are diffusion controlled.

In the present study we report about further experiments performed to a) determine the *reaction products*, and b) confirm the *role of the support* in the diffusion control.

2. Experimental and results

Details of the reagents and materials used and of the experimental procedure for the kinetic studies have been already reported³).

a) Reaction Products. To identify the reaction products, thermal treatments of the pure DF and activated carbon, of the synthetic mixtures and of untreated fly ash are performed in a closed tube using a set-up represented in Figure 1. Samples were treated in closed tube for 2 h; after the treatment, nitrogen (100 ml/min) flows through the tube for 1 h, bubbling in a series of five impingers, the first filled with cyclohexane, the following four with a saturated $Ba(OH)_2$ solution. Preliminary experiments showed that one impinger filled with cyclohexane and four impingers filled with saturated $Ba(OH)_2$ solution are sufficient to collect the organics and the carbon dioxide developed in the reaction conditions.

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dioxide developed in the reaction, the four $Ba(OH)_2$ solutions and a blank are titrated with HCl 0.5 N. The residual TOC content of the sample is determined.

Table 1 shows the distribution of the products in the different reactions. For DF, both as a pure compound or in a mixture with SiO_2 , the only product is the reactant, recovered in the organic solvent. For activated carbon, a single product is found, carbon dioxide. For the reactions of fly ash at 250°C and 325°C, CO_2 is the main product; tetra- to hexachlorobenzenes have been detected in the impinger with the organic solvent, but until now not quantified. At higher temperatures (500°C), CO_2 is the only product.

Table	1.	Products	of the	thermal	treatment	of pure	compounds,	synthetic	mixtures	thereof	or
		fly ash in	closed	tube at	different	temperati	ures ^a .	•			

sample	T (°C)	TOC(t=0)	TOC(t=2h) (%)	CO ₂ (%)	Organics (%)	Recovery %
DF	75	9 10 ⁵	-	-	99	99
DF/SiO ₂	56	3770	100	-	1 ^b	101
DF/SiO ₂	75	5890	95	-	17 ⁶	112
DF/SiO ₂	150	3770	45	-	44 ^b	89
C C/SiO ₂ C/SiO ₂	400 350 400	10 ⁶ 1350 1350	44 91 67	48 18 44	- -	92 109 111
C/SiO ₂	550	1350	0	100	-	100
fly-ash fly-ash fly-ash	250 325 500	4790 4790 4790	71 69 6	15 10 94	(c) (c) -	92 79 100

(a) Reaction product data are given in % of the initial TOC.

(b) Organics = DF

(c) Tetra- to hexachlorobenzenes were detected, but not quantified.

b) Role of the Support. In order to gain information on the role of the support, the behavior of pure DF and activated carbon was also studied. The reaction temperature ranged from 57 to 150°C for pure DF, from 325 to 600°C for pure activated carbon; the reaction times varied from 15 to 240 minutes. The results are reported in Tables 2 and 3. The data for the runs on the pure compounds were fitted with a first-order kinetic equation. The rate constants (min⁻¹) are shown in Figure 2a-b, as Arrhenius plots together with the Arrhenius plots obtained for the reaction of the SiO₂-mixture of the compounds³⁾. Table 4 reports the activation parameters.

3. Discussion and Conclusions

DF undergoes a physical transformation from solid to gaseous state (Table 1) accrding to a pseudo-first order kinetic. For activated carbon, the reaction is a combustion to gaseous CO_2 (Table 1) following a pseudo-first order kinetic.

Looking at the Arrhenius plots (Figure 2), a linear trend is observed for pure DF and activated carbon reactions, while a non-linear trend, depicted as two connected straight lines with different slopes, is observed for the synthetic mixtures reactions. To explain this behavior, we hypothesize a physical and/or chemical adsorption of DF or carbon on the surface and in the pores of SiO₂. At lower temperatures, the rate-limiting step is the desorption of DF from the surface or the combustion of carbon to CO_2 . At higher temperatures, the rate-limiting step is the diffusion of DF or CO_2 through the pores of the

support.

On the basis of this hypothesis and according to the calculated activation parameters (Table 4) for fly ash, both reactions R1 and R2 are confirmed to be diffusion controlled. One of 4) for fly ash, both reactions R1 and R2 are confirmed to be diffusion controlled. One of the two reaction, probably R1 having the higher apparent activation energy, could correspond to the carbon oxidation to CO_2 ; the other could be a desorption of polychlorobenzenes. Results obtained for the SiO₂ mixtures point out the important role of the supprt in determining kinetics and mechanism of these reactions. This hypothesis will be further tested: other batch experiments with different starting carbon content and runs on a continuous flow apparatus are needed.

Table 2. Thermal treatment of pure DF: DF (mg) - time data at different temperatures.

t(min) T(°C)	0	15	30	60	90	120	150	180	210	240
57 68 75 87 100 125 150	368 102 304 100 110 100 112	26 18	330 236 59 33 2	321 70 160 44 20	256 146 6	217 45 122 10	196 86	183 25 86 4	164 47	134 8 36

Table 3. Thermal treatment of pure activated carbon: C (mg) - time data at different temperatures.

t(min) T(°C)	0	15	30	60	90	120	150	180	210	240
325 350 375 500 600	98 201 101 99 250	21	92 83 14 2	87 154 64 2	86 56	76 144 45	69 36	69 110 30	66 21	64 83 17

Table 4. Activation parameters: ΔE^{\ddagger} (kcal mol⁻¹) and ln A.

	DF-SiO ₂ ³⁾	pure DF	C-9	SiO ₂ ³⁾	pure C	Fly	Ash ³⁾
	50-75°C 75-200°C	57-150°C	325-375°C	375-600°C	325-600°C	Rl	R2
ΔΕ‡	23.58 5.947	11.89	59.98	7.884	16.89	6.780	3.240
lnA	23.2 -2.07	12.7	36.6	-4.19	8.03	-5.78	-5.77

5. References

- 1) For a short review of general references, see: Lasagni M., G. Moro, D. Pitea, and L.
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Figure 1. Apparatus for the identification of the products.



Figure 2a. Arrhenius plots for the reactions of pure DF (+) and DF-SiO₂ mixture³⁾ (**■**)



Figure 2b. Arrhenius plots for the reactions of pure Carbon (+) and C-SiO₂³ mixture (**■**)

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