# CONTROLLING PCDDAPCDF EMISSIONS FROM INCINERATORS BY FLUE CASCLEANING\*

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### ABSTRACT

New source performance standards for municipal waste combustors (MWCs) and guidelines for existing incinerators in the U.S., proposed on December 20, 1989, are to be promulgated in December 1990. The proposed national regulations require more stringent control of particulate matter and include pre-combustion, combustion, and post-combustion controls, the last two depending on size and age of the facility.

Dry scrubbing processes have been used exclusively on recent MWCs and are planned for future MWCs in the U.S. for fine gas cleaning (post-combustion control). They inherently include particulate manticulate manticulate of a series and a series of the process of

## INTRODUCTION

The combustion of municipal solid waste (MSW) in the U.S. has almost doubled in the past 3 years, with waste-to-energy conversion complementing the reduction of waste volume for landfill disposal. About 15% of the MSW generated is incinerated, equivalent to 68,000 tonnes/day. Since 95% of the MSW burned is in waste-to-energy facilities, the test results reported here will be for municipal waste combustons (MWCs) with energy recovery.

Over the same 3 years, the U.S. Environmental Protection Agency (EPA) has been developing stricter rules to control pollutant emissions from MWC facilities. On December 20, 1989, these rules were proposed for new facilities [new source performance standards (NSPS)] and existing facilities (emission guidelines). They require all facilities to use three complementary methods to control air polluting emissions: material separation (pre-combustion fuel cleaning), combustion control [good combustion practice (GCP)], and post-combustion control or fine gas cleaning (FGC). The final rules, to be promulgated in December 1990, are now being prepared following the public comment period and the consideration of additional data.

While the present rule for MWCs requires only particulate matter (PM) control, the proposed rules also limit "MWC emissions," mirrogen oxides (NO<sub>X</sub>), and carbon monoxide (CO). "MWC emissions" include "MWC metals" as measured by total polychlorinated dibenzo-p-dioxins (PCDD) and dibenzofurans (PCDD), and "MWC acid gas" as measured by hydrogen chloride (HCI) and sulfur dioxide (SO2). Table I summarizes the proposed emission limits for these air pollutants, the limits being a function of the facility's size (capacity) and age (new or existing unit). I While all facilities must comply with PM, PCDD/PCDF, and CO limits, the acid gas emission limits apply to all but small existing sources (\$225 tomes/day). Only large new sources (\$225 tomes/day) must achieve the NO<sub>X</sub> emission limits. While only the proposed MWC emission limits (except CO) are given in Table I, the proposed rules also cover personnel training and operating and monitoring requirements for each facility to ensure compliance with emission limits.

<sup>\*</sup> This paper has been reviewed in accordance with the U.S. Environmental Protection Agency's peer and administrative review policies and approved for presentation and publication.

TABLE I. PROPOSED MUNICIPAL WASTE COMBUSTION EMISSION STANDARDS<sup>2,1</sup>

	New Source Performance Standards (NSPS)		Emission Guidelines		
CAPACITY, tonnes/day (tons/day)	≤225 (≤250)	>225 (>250)	≤225 (≤250)	>225,≤2000 (>250,≤2200)	>2000 (>2200)
METAL EMISSIONS  Particulate Matter, mg/dscm (gr/dscf)  Opacity, %	34 (0.015) 10	34 (0.015) 10	6 <del>9</del> (0.030) 10	69 (0.030) 10	34 (0.015) 10
ORGANIC EMISSIONS -Chlorinated Dibenzo-p-dioxins & Dibenzofurans (PCDD/PCDF), ng/dscm	75 250 <sup>c</sup>	5-30b	500 1000°	125 250°	5-30b
ACID GAS CONTROL, %, OR EMISSIONS (ppmv) -HCI -SO2 aNO <sub>x</sub>	80 (25) 50 (30) None	95 (25) 85 (30) (120-200) <sup>b</sup>	None None None	50 (25) 50 (30) None	95 (25) 85 (30) Nonc

<sup>\*</sup>All emission limits are referenced to dry gas with 7% O2 concentration (20°C, 101.3 kPa).

Dry acid gas scrubbing processes (or dry scrubbers) for FGC are used on the more recent MWC facilities in the U.S., and this trend is expected to continue for units now being planned. The dry acid gas FGC processes convert the acid gases to a solid form which can be collected as PM. Similarly, organics and metals as solids prior to or after scrubbing are also collected as PM.

Since the main focus here is on controlling PCDD/PCDF, FGC process conditions affecting their control as PM will be discussed, and test results mainly from compliance tests will be compared with the proposed U.S. rules. The potential effects of material separation and NO<sub>X</sub> control on PCDD/PCDF and PM emissions will not be discussed. Data are not available on these effects, but properly controlled arumonia flows (minimum slip) in non-selective and selective catalytic reduction are believed to have little or no effect on PCDD/PCDF and PM emissions from dry scrubbers. The treatment or disposal of ash or solid residue will not be discussed as this waste is subject to solid waste rules in the U.S.

# DRY FLUE GAS CLEANING

Dry acid gas control processes on MWCs produce a dry powdery waste, and flue gases leaving these processes are not saturated with water. In contrast, wet processes discharge slurries and flue gases saturated with water. Two dry processes are applied on MWCs: dry sorbent injection (DSI) into flue gas followed by PM collection, usually by a fabric filter (FF), and spray dryer absorption with either a FF or an electrostatic precipitator (ESP) for PM collection. While designed primarily to remove HCI and SO2, both processes achieve multi-pollunat control, including PM, trace organics, and race heavy metals. In wast-to-energy MWCs with dry scrubbers, the flue gas leaves the boiler at 200°C or less and enters the PM collector at 150°C or less. Therefore, the net production of PCDD/PCDF by de novo synthesis in the PM collector would not be a problem.

bSingle value, probably in this range, will be supplied at promulgation of rules.

Value for refuse-derived fuel (RDF) combustors in the capacity category shown.

Figure 1 shows the DSI process with two options. The dirty flue gas may be hamidified and cooled via water injection prior to its contacting powdered sorbent [usually hydrated lime, Ca(OH)2] in a reactor, or it may be cooled indirectly using a heat exchanger before sorbent injection. Both options reduce the gas temperature to about 150°C and lower the approach to saturation temperature (difference between temperature of the gas and its dewpoint) to enhance the acid-gas/sorbent reaction.

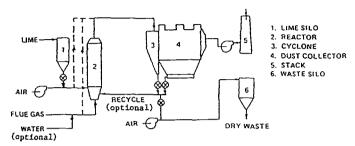


Figure 1. Dry sorbent injection into fluid bed reactor or flue gas duct (dashed line).

Several plants, generally with combustors rated at 180 tonnes/day or less, use the DSI/FF system. Ca(OH)2 is the sorbent for each plant.

The lime spray dryer absorber (SDA) in combination with PM collection is shown in Figure 2. Five gas at about 200°C enters the SDA and is cooled to around 140°C as the Iime sturry droplets are dried in contact with the horter gas. The gas/lime sturry reaction leads to neutralization of the acid gases and production of solids. Since the gas into the SDA is sprayed with a wet sorbent sturry or solution and, while the collected solids in the process are dry, this process is sometimes referred to as a semi-dry rather than a dry process.

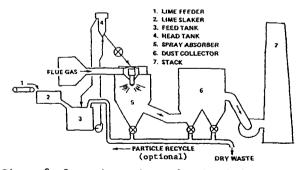


Figure 2. Spray dryer absorption (semi-dry) process.

Most recent MWCs having over 180 tonnes/day capacity and those now being planned for the U.S. use the SDA/FF or SDA/ESP system for acid gas control. As with the DSI/FF system, the approach to saturation temperature and reagent (or stoichiometric) ratio (moles of sorbent per mole of acid gases entering the scrubber) are the major parameters affecting acid gas removal.

PCDD/PCDF removal in dry scrubbers is enhanced by lower gas temperature which leads to condensation of vapor and improved adsorption onto particles, especially fine particles. The presence of lime-based sorbents may also enhance the removal of PCDD/PCDF, by providing additional particle surface area from the reaction products for adsorption, chemical reaction, or both. The limited vapor pressure data on chlorimated dioxing suggest that condensation of these compounds is not their sole mechanism of removal. The carbon (C) content of the flyash particles appears to affect PCDD/PCDF capture. A recent patent proposes the addition of activated C to flue gas to improve removal of PCDD/PCDF (as well as NO<sub>X</sub> and mercury (Hg)).

## TEST RESULTS AND COMPARISON WITH PROPOSED RULES

Test results from facilities with dry scrubbers are shown in Tables II and III. These results indicate that only SEMASS Unit 2 had a greater average PCDD/PCDF emission (311 ng/dscm) than the proposed limit (125 ng/dscm, see Table I). While this average is based on three tests, with emissions of 18.0, 6.6, and 907 ng/dscm, respectively, no explanation was given for the highest value reported or any mitigating factors. Limited test data indicate that the lime SDA/EF system is more effective in controlling PCDD/PCPF emissions than the lime SDA/ESP system. This may be a result of better fine particle collection in the FF and/or secondary absorption/adsorption in the filter cake. The available PM control data show that, except for the SDA/ESP system, good PM control (>99%) parallels high PCDD/PCDF control (>95%). However, all PCDD/PCDF data in Table III meet the proposed emission guidelines, since all facilities listed have capacities below 2000 tonnes per day.

TABLE IL. CONTROL OF PARTICULATE MATTER (PM), POLYCHLORINATED DIBENZO-P-DIOXINS (PCDD) AND DIBENZOFURANS (PCDF), AND SELECTED HEAVY METALS WITH DRY LIME INJECTION/FABRIC FILTER SYSTEMS<sup>4,5</sup>

Location and Test Date	Average PM ( mg/dscm @		Average Total PCDD/PCDF Concentration ng/dscm @ 7% O	
	inlet	outlet	outlet	
-Claremont, NH				
Unit 1. 5/87	NAb	25	NA.	
7/87	ŇA	NA	37.6	
Unit 2, 5/87	NA.	9.8	NA.	
7/87	NA	NA	32.3	
St. Croix, WI				
6/88	NA	34	7.73	
10/88	NA	34 27	NA	
Springfield, MAC				
7/88	2059	3.7	0.15d	
Dutchess County, NY				
Unit 1, 2/89	NA	22	4.83	
Unit 2, 2/89	NA	80	17.9	
3/89	NA	25	NA.	
5/89	NA	18	NA	

<sup>\*</sup>dscm = dry standard cubic meter (20°C, 101.3 kPa).

bNot available or not measured.

<sup>&</sup>lt;sup>c</sup>All concentrations are referenced to dry gas with 12% CO<sub>2</sub>.

<sup>&</sup>lt;sup>d</sup>Dioxin at cordet reported as 2,3,7,5 tetrachlorinated dibenzodioxin equivalent (EPA method).

# TABLE III. CONTROL OF PARTICULATE MATTER (PI (PCDD) AND DIBENZOFURANS (PCDP), AND S SPRAY DRYER ABSORBER (SDA SDAJELECTROSTATIC PRECIPITA

	Average PM (mg/dscm @	Average PM Concentration <sup>a</sup> mg/dscm @ 12% CO <sub>2</sub>		PCDD/PCDF ration 0 7% O2
Location, Control System, and Test Date	inlet	outlet	inlet	outlet
•Marion County, OR Unit 1, SDA/FF 9/86	2016	5.3	43.0	1.26
•Biddeford, ME Unit A, SDA/FF 12/87	7322	32	903	4.38
•Mid-Conn.b Unit 11, SDA/FF 7/88 2/89	5514 4073	9.2 4.1	996 747	0.646 0.368
•Millbury, MA Unit I, SDA/ESP 2/88 Unit 2, SDA/ESP 2/88	NA <sup>d</sup> NA	4.1 19	NA 170	NA 59.2
SEMASS Unit 1, SDA/ESP 3/89 Unit 2, SDA/ESP 4/89	9793 8832	18 27	NA NA	9.3 311c

dNA = not available or not measured. Average value of 18.0, 6.6, and 907.

Tables IV and V compare PCDD/PCDF emissions systems on a toxic equivalency basis. Table IV shows that the EPA method gave values below those from the International (1989) method. It also shows that the ratio of the total outlet PCDD/PCDF to toxic equivalency varies greatly, so that it is not possible to simply and easily convert from total PCDD/PCDF to toxic equivalencies, given one or the other. Table IV also shows that the total PCDF exceeded the total PCDD, except for the toxic equivalents for the mass burn combustor with the SDA/FF system. Table V indicates that the reported units with SDA/FF systems met the 0.1 ng/Nm<sup>3</sup> toxic equivalent (I-89) standard used in some European countries, while the units equipped with other PGC systems did not.

TABLE IV. COMPARISON OF TOTAL PCDD/PCDF AND 2,3,7,8 TCDD TOXIC EQUIVALENTS
(All concentrations are in ng/dscm referenced to dry gas at 20°C with 12% CO2.)

		Total P	Total PCDD/PCDF Toxic Equivalent Method®			Ratiob	
Combustor Type	Flue Gas Cleaning System	A. inlet	B. outlet	C. EPA	D. I-89	B/C	B/D
Mass Burn	SDA/FF	70.8 (26 <u>.5/44.2)</u> c	2.20 (1.01/1.19)	0.063 (0.060/0.002)	0.079 (0.072/0.006)	35	28
Mass Burn	SDA/ESP	279 (50.6/228)	76.0 (15.6/60.4)	0.485 (0.247/0.278)	1.159 (0.247/0.911)	157	66
Refuse De- rived Fuel	SDA/FF	996 (328/668)	0.646 (0.271/0.375)	0.0017 (0.000/0.0017)	0.0050 (0.0008/0.0042)	380	129
Processed Fuel	SDA/ESP	NR <sup>d</sup> (NR)	8.65 (NR)	0.105 (NR)	0.142 (NR)	82	61

EPA = U.S. Environmental Protection Agency, I-89 = International Method, 1989.

dNR = Not reported.

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discrete fly standard cubic meter (20°C, 101.3 kPa).
h All concentrations are for dry gas with 12% CO2.
Values are averages for normal SDA/EF temperatures (performance tests 6, 8, 12, 13, and 14).

<sup>&</sup>lt;sup>b</sup>Rutio is the total PCDD/PCDF value in column B to tonic equivalent value in column C or D.

<sup>&</sup>lt;sup>o</sup>Values in parentheses are total PCDD and PCDF, respectively.

# TABLE V. 2,3,7,8 TCDD TOXIC EQUIVALENTS (All concentrations are in ng/Nm<sup>3</sup> referenced to dry gas at 0°C with 11% 0/2°L)

Combustor Type	Flue Gas Cleaning System	2,3,7,8 TCDD Toxic Equivalentb		
		EPA	1-89	
Mass Burn	D\$I/FF	0.116	NA	
Mass Burn	SDA/FF	0.049	0.061	
Mass Burn	SDA/ESP	0.377	0.900	
Refuse Derived Fuel	SDA/FF	0.0013	0.0037	
Processed Fuel	SDA/ESP	0.0815	0.110	

<sup>&</sup>lt;sup>2</sup>Conversion from 12% CO<sub>2</sub> to 11% O<sub>2</sub> assumes % CO<sub>2</sub> + % O<sub>2</sub> = 21.

### SUMMARY

Dry scrubbing processes are widely used on modern MWCs in the U.S. The lime SDA in combination with a FF or ESP is the predominant system, with the hydrated lime DSI/FF system being applied on several small units (<180 tonnes/day). Generally, existing MWCs with dry acid gas control are achieving the proposed PCDD/PCDF emissions and greater PCDD/PCDF removal than the SDA/EF system. For the FGC systems compared, only the SDA/FF systems complied with the 0.1 ng/Nm<sup>3</sup> toxic equivalency (1-89) standard of some European countries.

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bEPA = U.S.Environmental Protection Agency, I-89 = International Method, 1989.